# Empirical Modeling of an *In Vitro* Activity of Polychlorinated Biphenyl Congeners and Mixtures

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The goal of this research is to predict an in vitro activity of polychlorinated biphenyl (PCB) congeners and their mixtures and to describe the relationship between this activity and chemical structure. The test system used multiple PCB concentrations on each cell culture plate in a repeated measures design, which improved precision for comparing between concentration levels. A weighted regression that accounted for this experimental design feature was used in fitting a nonlinear dose-response exponential model to the PCB concentration-activity data from an in vitro test system in which 3H-phorbol ester binding was measured in cerebellar granule cells exposed to different PCB congeners to test for their effects on protein kinase C translocation. The model allowed for the minimum level to be less than control, a common slope, and the estimation of the log of the concentration that produces an activity 50% above the control activity (E50) for 36 congeners and 3 commercial mixtures. Next, a weighted logistic regression using a second order response model in the variables Cl<sub>ortho</sub>, Cl<sub>para</sub>, and Cl<sub>meta</sub> was used to relate the estimated log E50s to indicators of chemical structure. This model was preferred over models that might seem more mechanistically based because in internal validation, it attained a smaller PRESS statistic (the sum of squares between all observed and predicted observations) than other models. Evidently, this second order model makes more efficient use of parameters than other models considered. Plots of the predictions of the logistic second order response model versus log  $K_{\rm ow}$  confirm the usual pattern that congeners with intermediate levels of log  $K_{\rm ow}$  are the more active. The data of three commercial mixtures were included in this regression by assuming a common combination index (ratio of observed E50 to predicted E50, assuming dose addition). The logistic model suggests that congeners with one, two, or three chlorine substitutions at the ortho position are more active than other congeners. Also, congeners with log  $K_{ow}$  between 5.2 and 6.6 are generally more active. The estimated combination index indicated that the joint action of PCB congeners in the three commercial mixtures was less than dose additive. The error sum of squares was significantly large, which may indicate a lack of fit of the logistic model. Empirical Bayes estimates (EBE) are weighted averages of model predictions and observations of E50s and can be better estimates than the fitted model when there is a lack of fit. The PRESS statistic for the EBE indicated larger prediction error than for the logistic model, but the EBE provided better estimates of commercial mixture E50s based on dose addition. This may indicate that the logistic model is not incorporating all the information in the single congener data needed to predict mixtures. Key words: empirical model, in vitro activity, neurotoxicity, polychlorinated biphenyls, repeated measures design.

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Polychlorinated biphenyls (PCBs) are industrial compounds detected in air, water, sediments, fish, wildlife, and humans (1,2). PCBs are prepared by the chlorination of biphenyls, and the result is a mixture of possibly as many as 209 congeners. Although the manufacture of PCBs has been banned in the United States, these compounds remain a serious environmental pollutant due to ongoing release from hazardous waste sites, the accidental breakdown of electric transformers, and the high resistance to degradation.

Risk assessment of PCBs currently involves usage of toxic equivalency factors (TEFs), which are predicted on the assumption that this class of chemicals elicits their toxic responses through a common receptormediated mechanism. Structure—activity relationship studies, for example, have found that PCB-induced body weight loss, thymic

atrophy, immunotoxicity, endocrine and reproductive toxicity, and carcinogenicity are associated with high affinity for the aryl hydrocarbon (Ah) receptor (3). Recent studies, however, have shown environmentally relevant *ortho*-substituted PCB congeners with weak or no Ah-receptor activity have effects on brain dopamine concentrations in vivo (4) and in vitro in PC12 cells (5). Kodavanti et al. (6) have also found that ortho-substituted PCB congeners have significant effects on calcium homeostasis mechanisms in vitro, while non-ortho PCBs, having a more coplanar structural configuration, are relatively inactive in vitro.

This paper builds on the previous work of Kodavanti et al. (6) by developing an empirical model for predicting the *in vitro* activity of PCB congeners. This information may be useful in developing a risk

assessment strategy for nondioxinlike PCBs and their mixtures. The activity was measured in an *in vitro* test system in which different PCB congeners and PCB mixtures were tested for their effects on protein kinase C (PKC) translocation by measuring <sup>3</sup>H-phorbol ester binding in cerebellar granule cells (6,7). The prediction of the activity of PCB mixtures is based upon knowledge of the chemical composition and the *in vitro* activity of the components of the mixture.

We considered using the logistic dose-response model to determine the effective concentration that produces an activity 50% above the control activity (E50s) for 36 tested congeners and the 3 commercial mixtures. The logistic model involves the estimation of a minimum and a maximum activity. However, estimates of the maximum were quite variable because not all congeners attained maximum activity. The exponential model is similar to the logistic model but has no maximum value so this model was used instead. Logs of the mean activity relative to control activity were fit to an exponential model using the data from 36 congeners and the 3 commercial mixtures; the model had a common slope parameter, a common minimum value, and a separate log E50 for each of the congeners and the commercial mixtures. There is a correlation between the observed activity values from the same congener due to variability between culture plates. The use of weighted regression based on variance components estimated from the repeated measures design permitted data from all congeners to be estimated simultaneously while addressing this

Address correspondence to D.J. Svendsgaard, 8874 Lansdowne Drive NW, Calabash, NC 28467 USA. Some of this work was done while D.S. was a member of the Health Effects Research Laboratory. Chris Waller provided valuable insight to this project. We thank Mats Tysklind of Umea University, Sweden, and Subash Basak of National Resources Research Institute, Duluth, Minnesota, for their excellent comments on the earlier version of this manuscript. The research described in this article has been reviewed by the National Health and Environmental Effects Research Laboratory, U.S. Environmental Protection Agency, and approved for publication. Approval does not signify that the contents necessarily reflect the views and policies of the agency nor does the mention of trade names or commercial products constitute endorsement or recommendation for use. Received 27 December 1996; accepted 13 August correlation. The weights formed a block diagonal matrix. The minimum value of the dose–response curve was allowed to be negative (less than control) in view of the recent interest in U-shaped dose–response curves (8).

Next, a structure-activity relationship needed to be developed so that the E50s of the untested congeners could be estimated. After considering various models involving  $\log K_{ow}$  and indicators of chemical structure, we decided to approximate this relationship by a logistic second order response surface model in the variables  $\text{Cl}_{ortho}$ ,  $\text{Cl}_{para}$ , and  $\text{Cl}_{meta}$ . This model was fit to the logs of the E50s using weighted nonlinear regression. The logs of the E50s of the three commercial mixtures were simultaneously fitted in this regression through the use of the dose-addition equation. For these mixtures, a single combination index was also estimated. The combination index is the ratio of the E50 of the mixture to the E50 predicted by the doseaddition assumption. The reason for simultaneously estimating the structural activity relationship and the mixture E50s was to constrain the estimated structural relationship to one capable of predicting the activity of mixtures based upon dose additivity.

It is ideal to develop a model with one set of data and validate the model with a second set of data; this validation process is called external validation. In this case, all the data were needed to develop the model due to the small sample size; therefore, the model was internally validated. Internal validation involves excluding one data point at a time from the model fitting process and comparing the resultant prediction of the excluded point with the observation of that point. After each observation has been excluded and predicted, the sum of squares of the prediction differences is called the PRESS statistic. The lower the PRESS statistic the better the model.

The PRESS statistic was calculated for five models, and most of them were more biologically based than the second order model. Hansch, the father of quantitative structure-activity relationships (QSAR), derived a quadratic polynomial to relate biological activity to log P (9). Therefore, one model we considered was a quadratic model in  $\log K_{ow}$ . The quadratic coefficient was fixed and the linear coefficients were allowed to vary with Cl<sub>ortho</sub>. The intercepts varied with the main effects of Cl<sub>ortho</sub> and Cl<sub>para</sub> There were biological reasons for believing that Clortho is an important variable, but the reason for considering Cl<sub>para</sub> was more empirically based. A main effects model was also fit using dummy variables that considered Cl<sub>ortho</sub>, Cl<sub>para</sub>, and Cl<sub>meta</sub> to be factors. The second order logistic model attained a smaller PRESS value than other models.

In choosing the model we were guided by the PRESS statistic and how well the E50s of the mixtures were predicted. The data contain more information about the activity and chemical structure relationship than we have modeled. This state of affairs is due to our search for the most detailed model that could be validated with this sample size. Also, the PRESS statistic seems to favor models that use continuous independent variables rather than dummy variables such as would be used to describe a main effect model in the factors CL are and Clarge.

the factors CL<sub>ortho</sub>, Cl<sub>para</sub>, and Cl<sub>meta</sub>. These efforts are preliminary in some ways. The use of physicochemical variables as independent variables may further explain these activity data. However, considering the prevalence of mixtures in the environment, our focus is on the prediction of the activity of mixtures. This work is a step in that direction, and it gives a framework for more detailed structural-activity research to build on.

Our avoidance of physicochemical variables at this stage of the research is based upon three reasons. First, the selection of congeners to test was based mainly on their presence in environmental mixtures; therefore, the sample of congeners is unlikely to be ideal for the determination of a mechanistically based model. Second, there is measurement error in these variables. Sabljiĉ (10) has described the measurement error in log  $K_{ow}$  and has concluded that the use of the noctanol/water partition should be avoided in environmental research. Approaches using physicochemical variables as independent variables in regression routines need to address this error. The practice of combining several physicochemical variables into a summary variable using principle component analysis does address the measurement error problem. Third, most biologists do not think in terms of physicochemical variables and describe their results in terms of indices of structure, such as we use here. For example, Kodavanti et al. (11) has found that noncoplanar congeners are usually more active. Noncoplanarity is related to the configuration of the ortho substitutions. Our descriptive approach sheds light on the importance of such theories in explaining the variation of the E50 estimates.

The success of our approach depends on an assumption of smoothness of the E50 response surface. For example, the logistic second order model can estimate at most one peak in a response surface that might not be very smooth. Our approach should be judged on its clarification of important aspects of the E50 response surface, on its ability to predict mixtures, and on its ability to indicate how future experiments can be designed to improve mixture prediction.

We also present some results based upon empirical Bayesian analysis. This approach can fit response surfaces that are less smooth than the logistic second order model can fit.

# Materials and Methods

The in vitro test system. The in vitro test system of Kodavanti et al. (6,7) measures increases in [3H]-phorbol ester (PDBu) binding, which suggests increased activation/translocation of PKC from cytosol to the membrane. Translocation of PKC is dependent on the concentrations of intracellular free Ca2+ and/or diacylglycerol (12,13). PKC has been reported to play a key role in a number of physiological and toxicological phenomena (14,15). Cerebellar granule cells grown on 12-well culture plates were tested after 7 days in culture for [3H]-PDBu binding. Each replicate consisted of a control and usually six different concentrations placed in the wells of the cell culture plates. Generally, four replicates were used and, other than control, the concentrations of PCBs were 1, 3, 10, 30, 50, and 100 µM. Table 1 shows the details of the experimental designs.

Chemicals and terminology. Figure 1 shows the chemical structure of a PCB congener and explains how the congeners are denoted. The log of the octanol-water partition coefficient is denoted by  $\log K_{\text{ow}}$  and was obtained from Hawker and Connell (16). The tested congeners are listed in Table 1. The percentages in the commercial mixtures were the averages across lots of values from Frame et al. (17).

The concentration–activity model. The log<sub>10</sub> of activity ([<sup>3</sup>H]-PDBu binding) relative to control and averaged across culture plates was fit to an exponential concentration–activity model. Specifically, the model for the *j*th congener was

$$y = m_0 + (k - m_0) e^{s \left[ (\log_{10} C) - \log_{10} E50_j \right]}$$
 (1)

where y is the average across plates of the  $\log_{10}$  of  $[^3H]$ -PDBu binding relative to the control activity, C is the concentration ( $\mu$ M), and  $k = \log_{10} 1.5$ . The parameter  $m_0$  is the log of the minimum of the concentration—activity model, and s is a slope parameter. This parameterization allows the standard error of the log E50 to be obtained directly from the nonlinear routine, which is based on the delta method.

This model was fit simultaneously to all the nonzero dose data from the 36 congeners and 3 commercial mixtures using weighted regression. The weights were determined as follows. A repeated measures analysis was done on the log of the activity relative to control for each congener. This resulted in

Table 1. Experimental conditions									
IUPAC	Structure	Log K <sub>ow</sub>	Plates	Low concentration (µM)	High concentration (µM)	Number of doses			
4	2.2	4.65	5	1	100	6			
11	3,3′	5.28	4	i	100	6			
14	3,5	5.20	4	i	100	6			
15	4,4	5.30	4	1	100	6			
19	2,2′,6	5.02	4	1	100	6			
21	2,3,4	5.51	4	3	100	6			
28	2,4,4	5.67	6	1	100	6			
47	2,2′,4,4′	5.85	4	1	100	6			
50	2,2′,4,6	5.63	4	1	100	6			
51	2,2′,4,6′	5.63	4	1	100	6			
52	2,2′,5,5′	5.84	4	1	100	6			
53	2,2′,5,6′	5.62	4	3	100	5			
54	2,2',6,6'	5.21	4	1	100	6			
77	3,3',4,4'	6.36	4	1	100	6			
80	3,3′,5,5′	6.48	4	1	100	6			
82	2,2′,3,3′,4	6.20	4	10	100	4			
85	2,2′,3,4,4′	6.30	4	10	100	4			
95	2,2′,3,5′,6	6.13	4	10	100	4			
99	2,2′,4,4′,5	6.39	4	10	100	4			
100	2,2′,4,4′,6	6.23	4	3	100	5			
101	2,2',4,5,5'	6.23	4	10	100	4			
104	2,2',4,6,6'	5.81	4	1	100	6			
105	2,3,3',4,4'	6.65	5	1	100	6			
110	2,3,3',4',6	6.48	4	10	100	4			
118	2,3',4,4',5	6.74	4	1	100	6			
126	3,3',4,4',5	6.89	4	3	100	4			
127	3,3',4,5,5'	6.95	4	3	100	5			
128	2,2',3,3',4,4'	6.74	4	1	100	6			
133	2,2´,3,3´,5,5´	6.86	3	1	100	6			
136	2,2´,3,3´,6,6´	6.22	4	1	100	6			
138	2,2^,3,4,4^,5^	6.83	4	10	100	4			
153	2,2′,4,4′,5,5′	6.92	4	1	100	6			
156	2,3,3´,4,4´,5	7.18	5	1	100	6			
169	3,3′,4,4′,5,5′	7.42	4	1	100	6			
179	2,2^,3,3^,5,6,6^	6.73	4	10	100	4			
180	2,2',3,4,4',5,5'	7.36	4	1	100	6			
AR1016	Mix	5.49 <sup>a</sup>	5	1	100	6			
AR1254	Mix	6.51 <sup>a</sup>	4	1	100	6			
AR1260	Mix	6.98ª	5	1	100	6			

IUPAC, International Union of Pure and Applied Chemistry. 
<sup>a</sup>Based on average of congeners present.

estimates for the variability due to plates, variability due to doses, and residual variability.

For the data from each congener (or mixture), a covariance matrix with plate variability at the off-diagonal elements and plate plus residual variability on the diagonal was formed. The weights for all the 36 congeners and the 3 commercial mixtures formed a block diagonal matrix. See Draper and Smith (18) for an explanation of why it is valid to use linear regression with such a weight matrix.

The dose-addition method of predicting the mixture E50. The E50 of a mixture satisfies the following equation when the joint action is dose addition:

$$\frac{1}{\text{E50}_k} = \sum_{j=1}^{209} \frac{\pi_{jk}}{\text{E50}_j},\tag{2}$$

where  $\pi_{jk}$  is the fraction of the jth congener

in the kth mixture. The combination index (19) is the ratio of the actual E50 of the mixture to the E50 predicted in Equation 2. Combination indices that are >1 indicate antagonism and those <1 indicate synergism.

The structure—activity model. Weighted nonlinear regression analysis was used to determine the relationship between the log of the E50 of the concentration—activity model and the chemical structure of the PCB congener. Also, the logs of the E50 for the three commercial mixtures were included in this regression by assuming that these mixtures all had the same combination index. The weights used were the reciprocal of the square of the estimated standard errors of the log E50s. The model used to relate the log E50 of each congener to the structure was the second order logistic model:

log E50 = 
$$m + (M-m)/(1 + \exp [\gamma_0 + \gamma_1(Cl_{ortho}-2) + \gamma_2(Cl_{para}-1)]$$

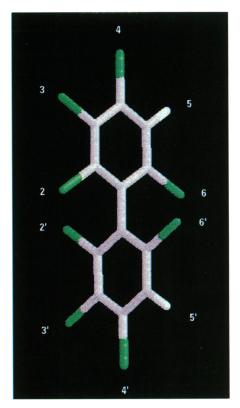


Figure 1. The chemical configuration of polychlorinated biphenyls (PCBs) for 2,2',3,3',4,4',6,6'. Green indicates the substitution of chlorine at the position and white indicates an unsubstituted position. PCB congeners have two rings, which can rotate around the bond connecting them. On each ring there are five positions where chlorine substitution can occur. These positions are numbered as shown. The *ortho* positions are 2,2',6, and 6'; the *meta* positions are 3,3',5, and 5'; and the *para* positions are 4 and 4'.

$$\begin{array}{l} + \gamma_{3}(Cl_{meta}-2) + \gamma_{11}(Cl_{ortho}-2)^{2} \\ + \gamma_{22}(Cl_{para}-1)^{2} + \gamma_{33} (Cl_{meta}-2)^{2} \\ + \gamma_{12}(Cl_{ortho}-2)(Cl_{para}-1) \\ + \gamma_{13}(Cl_{ortho}-2)(Cl_{meta}-2) \\ + \gamma_{23} (Cl_{para}-1)(Cl_{meta}-2)] \end{array} \tag{3}$$

The logistic model becomes flat as the value of the expression within the square brackets of the equation becomes either positively or negatively large. This feature restricts the predicted values to lie in the range from m to M (minimum to maximum), thus improving the stability of the predictions.

The prediction of mixture E50s. Using the combination index and Equation 2, the log of the E50 of the mth mixture can be expressed as

$$\log E50_{m} = \log CI_{m} - \log \sum_{i=1}^{209} \pi_{i} 10^{-\log E50_{i}}$$
(4)

where all logs are to the base 10 and  $CI_m$  is the combination index for the mth mixture. In fact, when one views each congener as a

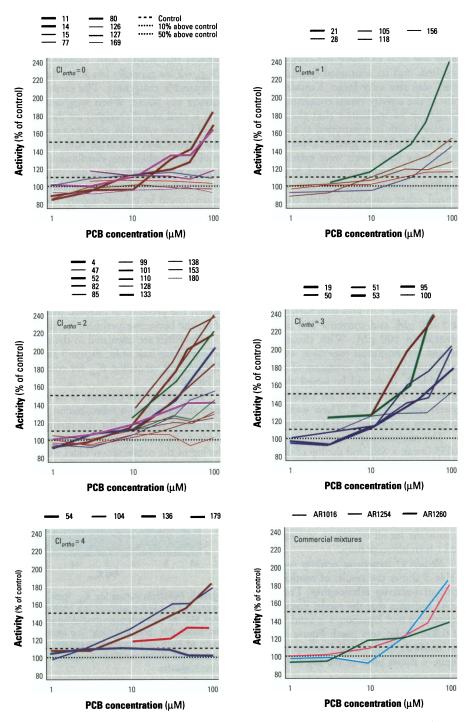


Figure 2. Activity—concentration curves. These curves show the average activity in percent control versus polychlorinated biphenyls (PCB) concentration for each of the congeners and the commercial mixtures. The color of the activity—concentration line represents the level of CI<sub>meta</sub>: blue is 0, green is 1, brown is 2, orange is 3, and purple is 4. The wider the activity—concentration line, the less chlorine at the *para* position. IUPAC, International Union of Pure and Applied Chemistry.

mixture having 100% of one congener ( $\pi_i$ = 1) and  $CI_m$ = 1, then the log of the E50s of the 36 tested congeners also satisfies Equation 4. The equation fit to the data was Equation 4, with Equation 3 substituted for log E50<sub>i</sub> in Equation 4.

Cross-validation. The PRESS statistic is the sum of squares of differences between

observed and predicted and is used for internal validation. The predicted are obtained for each observation by leaving out that observation from the regression routine, using the rest of the observations to fit the regression model, and predicting the deleted observation with the resultant fitted value. The  $Q^2$  statistic is 1-PRESS/PRESS<sub>0</sub>

where PRESS<sub>0</sub> is the PRESS statistic for an overall mean model using the same dependent variable. The  $Q^2$  statistic is similar to  $R^2$ . When  $Q^2$  is 1, the method has excellent internal validation. Unlike  $R^2$ ,  $Q^2$  can become negative for poor predictors. The  $Q^2$  statistic can also be computed for sets of data not used in the regression, and that statistic is called the  $Q^2$  for external validation. A weighted  $Q^2$  was also computed by weighting the sum of squares by the same weights used in the regressions.

Empirical Bayesian analysis. Bryk and Raudenbush (20) discuss empirical Bayesian analysis. Briefly, when data are analyzed by using a simple weighted linear regression with one continuous independent variable, the error sum of squares has a chi-square distribution, with degrees of freedom equal to the residual degrees of freedom if several conditions are met. These are 1) the elements of the dependent variable are normally distributed with a known variance, 2) the reciprocal of this variance is used as the weight, and 3) the dependent variable is linearly related to the independent variable. When this is the case, the empirical Bayes estimates (EBEs) of the true model can be used; they are points lying between the elements of the dependent variable and the straight line fitted by the regression. The smaller the error sum of squares, the closer the EBE is to the straight line.

We used the EBE in the case of weighted nonlinear regression with multiple independent variables. The weights must be estimated because the standard errors are unknown. Therefore, we expect the error sum of squares to be somewhat more variable than a chi-square distribution.

We tested 36 congeners so we could estimate their E50s directly. The E50 of the 173 untested congeners could be estimated from the fitted second order logistic model. By assuming there were indications of lack of fit of the model, we could use the EBEs in this case. However, EBEs only are known for the 36 tested congeners. To estimate the EBEs for the untested congeners, linear splines were connected to the EBE points to estimate the EBEs for the untested congeners. Those untested congeners with log  $K_{ow}$  values less (or greater) than the smallest (largest) tested congener were assigned the same EBE as the smallest (or largest) tested congener. These six groups were the coplanar congeners with  $Cl_{para} = 0$ ; the coplanar congeners with  $Cl_{para}$ = 1 or 2; the congeners with  $Cl_{ortho} = 1$ ; the congeners with  $Cl_{ortho} = 2$ ; the congeners with Cl<sub>ortho</sub> = 3; and the congeners with Cl<sub>ortho</sub> = 4.

The EBE for the *i*th observation (observed,) were obtained as follows:

 $EBE_i = \lambda_i observed_i + (1 - \lambda_i) fitted_i$ , (5)

where  $\lambda_i = \tau/(\tau + v_i)$ ,  $\tau$  is the unexplained variance between log E50s, v, is the estimated variance of the log E50 of the ith congener, and fitted; is the predicted value for the *i*th observation. The variance  $\tau$  was estimated by adding a constant to the reciprocal of the weights. This constant was increased until the error sum of squares was less than the 90th percentile of a chi-square with the residual degrees of freedom. This constant was used as the estimate of  $\tau$ .

### Results

Results of fitting an exponential concentration-activity model to 36 congeners and 3 commercial mixtures. Figure 2 shows the mean activity versus concentration over the region from 1 to 100 µM for the 36 congeners and 3 commercial mixtures. Note that 22 of the congeners have mean activities exceeding 50% of control. About 6 of the congeners barely exceed 10% of control.

Table 2. Estimates of log base 10 E50s from the

IUPAC	log E50	SE of log E50
4	1.531	0.111
11	1.488	0.085
14	1.848	0.102
15	3.148	0.546
19	1.689	0.140
21	1.354	0.064
28	1.936	0.118
47	1.792	0.113
50	1.504	0.069
51	1.467	0.081
52	1.341	0.065
53	1.220	0.061
54	1.842	0.353
77	2.832	1.190
80	1.819	0.114
82	1.300	0.099
85	1.412	0.089
95	1.194	0.089
99	2.125	0.143
100	1.985	0.080
101	1.659	0.102
104	1.627	0.112
105	1.808	0.116
110	1.241	0.036
118	2.326	0.170
126	2.055	0.554
127	2.468	0.099
128	2.269	0.199
133	2.077	0.172
136	1.645	0.154
138	2.215	0.142
153	2.247	0.142
156	2.602	0.217
169	3.660	0.837
179	2.104	0.092
180	4.381	1.964
AR1016	1.764	0.104
AR1254	1.798	0.081
AR1260	2.018	0.140

Abbreviations: IUPAC, International Union of Pure and Applied Chemistry; E50, the concentration producing an activity 50% above the control activity; SE, standard error.

A difficulty was encountered when fitting the exponential concentration-activity model (Equation 1) to the data. A very large log E50 estimate for congener 54 resulted, and its estimated standard error (SE) was also very large. Examining the plot of the activity versus concentration for congener 54 indicated that the activity decreased with concentration at concentrations of 30 µM and greater. Once the data from these dose levels were excluded, the nonlinear regression converged. Some large log E50 standard errors were also noted for several other congeners. Their concentration-activity relationships were also plotted, and decreasing activity at increasing concentration was also noted for those congeners. These data points were also excluded. Altogether, 9 of the 212 data points were excluded. These were congeners 54 and 77 and concentrations 30, 50, and 100 μM; congener 126 and concentrations 50 and 100 µM, and congener 169 and concentration 100 µM. With these points deleted, the nonlinear regression was stable and converged to the estimates of log E50 in Table 2. It should be noted that congeners 77, 126, and 169 are coplanar congeners with  $Cl_{para} = 2$ . There were 4 such congeners tested, and each was inactive.

The resultant slope estimate was 0.494 ± 0.033 (mean ± SE), and the log of the minimum  $m_0 = -0.0168 \pm 0.0079$ . The model for the ith congener is of the form log activity =  $-0.017 + s_i d^{0.494}$ , where the parameter s, can vary among the congeners and mixtures. On a log dose scale, the slope (0.494) is constant for all congeners and mixtures, and s; is an intercept term.

Results of structural activity modeling. Table 3 shows the results of modeling the structural-activity relationship. The  $Q^2$  of 0.641 indicates that the model described by Equation 3 and Equation 4 is valid. The  $R^2$ of 0.866 is also very good. Figure 3 shows the residuals of the model versus  $\log K_{ow}$ . Figure 4 shows plots of the log E50 versus

Table 3. Results of structural-activity modeling

 $\gamma_{12}$ 

 $\gamma_{13}$ 

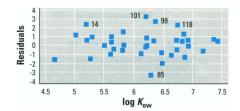
 $\gamma_{23}$ 

log<sub>10</sub> CI

 $\log K_{ow}$ . Generally, we expect to see activity decrease and then increase as  $\log K_{ow}$  increases. The plots show that the model generally reflects this shape. Also, congeners with Cl<sub>para</sub> = 2 are generally less active than other comparable congeners. The error sum of squares was 68.32. When weighted regression is used and the weights are the reciprocal of known variances, we expect under normal theory that this error sum of squares would have a chi-square distribution with 26 degrees of freedom. Since our weights are estimated rather than known, this sum of squares could be inflated slightly, but not to this amount. A simulation study indicated that using estimated weights based on t-distributions with 21 degrees of freedom would increase the 90th percentile about 10%. The 90th percentile of a chi-square with 26 degrees of freedom is 35.6. Factors that tend to increase this sum of squares are nonnormality, the presence of outliers, model lack of fit, and between-experiment variability.

The EBEs are calculated so there will be no significant lack of fit. Figure 5 shows the EBE plotted versus  $\log K_{ow}$  for comparison to Figure 4.

The ratio of the estimate to its standard error should follow a t-distribution with 26 degrees of freedom for the estimates in Table 3. Because the ratio corresponding to the log of the combination index exceeds 2,



**Figure 3.** Residuals versus log  $K_{\rm ow.}$  Residuals are (estimated log E50-predicted log E50)/standard error. E50, the concentration producing an activity 50% above the control activity. The International Union of Pure and Applied Chemistry (IUPAC) numbers are shown for those congeners with the larger residuals.

0.332

0.276

0.453

0.100

-1.363

-1.498

-1.511

2.931

**Parameters** Variables **Estimate** SE Ratio Minimum 1.142 0.196 5.824 М Maximum 3.274 1.169 2.801 Constant 2.442 0.875 2.790  $\gamma_0$ -0.379 -1.560 CI<sub>ortho</sub>-2 0.243  $\gamma_1$ Cl<sub>para</sub> -1 Cl<sub>meta</sub> -2 (Cl<sub>ortho</sub>-2)<sup>2</sup>  $\gamma_2 \\ \gamma_3$ -1.4730.887 -1.661 -0.7740.450 -1.720 -0.4040.260 -1.555γ11  $\gamma_{22}$ (CI<sub>para</sub> -1)<sup>2</sup> -0.858 0.524 -1.639 <sub>meta</sub> -2)<sup>2</sup> -0.544 0.338 -1.612  $\gamma_{33}$  $(Cl_{ortho}^{meta}-2) \times (Cl_{para}-1)$   $(Cl_{ortho}-2) \times (Cl_{meta}-2)$ 

Abbreviations: SE, standard error; CI, combination index.  $R^2 = 0.866$ ;  $Q^2 = 0.641$ .

(CI<sub>para</sub>-1) × (CI<sub>meta</sub>-2) log<sub>10</sub> CI

-0.452

-0.413

-0.684

0.293

the log of the combination index is significantly different from zero. This indicates that the mixtures are less active than predicted by the logistic model using dose addition.

Analysis of outliers. Two residuals were larger than 3 standard errors of the estimated log E50s. These were congener numbers 85 and 101. A plot of these residuals is shown in Figure 3. No observations were deleted from this regression analysis.

Table 4 shows the model predictions of the log base 10 E50s for all congeners together with the 95% confidence limits. Also shown are the log  $K_{ow}$ . Only three congeners were tested whose log  $K_{ow}$  exceeded 7. The large confidence limits of congeners with  $\log K_{ow}$  greater than 7 reflect the fact that the regression model is being extrapolated outside the experimental region to estimate the E50 of such congeners. Also shown in Table 4 are the EBEs for the log E50s. A value of 0.011 was estimated for  $\tau$ . The  $Q^2$ was 0.159, which is smaller than that obtained for the second order model, and indicates less predictability. To further evaluate the predictability of these estimates, the mixture E50s were calculated from the EBEs. The observed E50 for AR1016, AR1254, and AR1260 was 58.1, 62.9, and

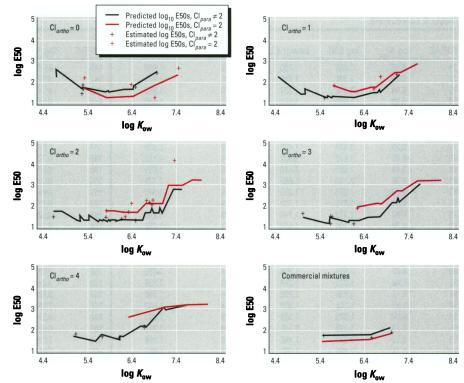


Figure 4. Predicted  $\log_{10}$  E50s versus  $\log K_{\rm ow}$  by  ${\rm Cl}_{ortho}$ . E50, the concentration producing an activity 50% above the control activity.

UPAC	log K <sub>ow</sub>	log E50	Lower CL	Upper CL	Empirical Bayes estimate	IUPAC	log K <sub>ow</sub>	log E50	Lower CL	Upper CL	Empirical Bayes estimate
1	4.46	2.338	1.678	2.999	1.370	36	5.88	1.535	1.358	1.713	1.750
2	4.69	2.201	1.615	2.787	1.638	37	5.83	2.079	1.621	2.536	2.326
3	4.69	2.566	1.848	3.284	2.517	38	5.76	1.505	1.302	1.708	2.351
4	4.65	1.691	1.395	1.987	1.603	39	5.89	1.505	1.302	1.708	2.305
5	4.97	1.468	1.325	1.611	1.370	40	5.66	1.238	1.107	1.369	1.365
6	5.06	1.468	1.325	1.611	1.370	41	5.69	1.280	1.195	1.365	1.358
7	5.07	1.732	1.369	2.095	1.370	42	5.76	1.280	1.195	1.365	1.342
8	5.07	1.732	1.369	2.095	1.370	43	5.75	1.238	1.107	1.369	1.344
9	5.06	1.468	1.325	1.611	1.370	44	5.75	1.238	1.107	1.369	1.344
10	4.84	1.691	1.395	1.987	1.558	45	5.53	1.278	1.165	1.391	1.294
11	5.28	1.601	1.406	1.796	1.638	46	5.53	1.278	1.165	1.391	1.294
12	5.22	1.721	1.367	2.076	2.517	47	5.85	1.781	1.612	1.949	1.798
13	5.29	1.721	1.367	2.076	2.517	48	5.78	1.280	1.195	1.365	1.337
14	5.28	1.601	1.406	1.796	1.638	49	5.85	1.280	1.195	1.365	1.798
15	5.30	2.593	2.006	3.180	2.517	50	5.63	1.431	1.323	1.538	1.481
16	5.16	1.289	1.190	1.388	1.483	51	5.63	1.431	1.323	1.538	1.481
17	5.25	1.441	1.301	1.582	1.462	52	5.84	1.238	1.107	1.369	1.323
18	5.24	1.289	1.190	1.388	1.464	53	5.62	1.278	1.165	1.391	1.244
19	5.02	1.514	1.290	1.739	1.580	54	5.21	1.621	1.237	2.004	1.614
20	5.57	1.292	1.197	1.387	1.589	55	6.11	1.317	1.236	1.397	1.931
21	5.51	1.348	1.253	1.444	1.370	56	6.11	1.317	1.236	1.397	1.931
22	5.58	1.348	1.253	1.444	1.625	57	6.17	1.326	1.216	1.436	1.928
23	5.57	1.292	1.197	1.387	1.589	58	6.17	1.326	1.216	1.436	1.928
24	5.35	1.289	1.190	1.388	1.438	59	5.95	1.238	1.107	1.369	1.667
25	5.67	1.348	1.253	1.444	1.954	60	6.11	1.699	1.491	1.907	1.931
26	5.66	1.292	1.197	1.387	1.917	61	6.04	1.317	1.236	1.397	1.935
27	5.44	1.289	1.190	1.388	1.417	62	5.89	1.280	1.195	1.365	1.745
28	5.67	1.972	1.672	2.272	1.954	63	6.17	1.317	1.236	1.397	1.928
29	5.60	1.348	1.253	1.444	1.698	64	5.95	1.280	1.195	1.365	1.667
30	5.44	1.441	1.301	1.582	1.417	65	5.86	1.238	1.107	1.369	1.785
31	5.67	1.348	1.253	1.444	1.954	66	6.20	1.699	1.491	1.907	1.926
32	5.44	1.441	1.301	1.582	1.417	67	6.20	1.317	1.236	1.397	1.926
33	5.60	1.348	1.253	1.444	1.698	68	6.26	1.317	1.236	1.397	1.923
34	5.66	1.292	1.197	1.387	1.917	69	6.04	1.280	1.195	1.365	1.550
35	5.82	1.505	1.302	1.708	2.330	70	6.20	1.317	1.236	1.397	1.926

(continued, next page)

UPAC   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   estimate   UPAC   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   estimate   UPAC   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   estimate   UPAC   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Estimate   UPAC   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Estimate   UPAC   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper CL   Og K <sub>m</sub>   Og E0   Lower CL   Upper	Table 4.	(continued)										
To   To   Sept   1.200	IUPAC	log K	log E50	Lower CL	Upper CL		IUPAC	log K	loa E50	Lower CL	Upper CL	Empirical Bayes estimate
72 6.26 1.356 1.26 1.486 1.486 1.592 141 6.62 1.665 1.380 1.590 2.185 7.73 6.04 1.228 1.1097 1.380 1.590 1.426 6.51 1.483 1.310 1.656 1.598 1.598 1.598 1.598 1.598 1.599 1.59	71			1 195			140					
73	72											
74 6.20 1893 1.481 1.937 1.926 143 6.60 1.483 1.310 1.856 1.989 75 6.05 1.781 1.781 1.782 1.939 1.937 1.44 6.23 1.966 1.410 1.922 1.821 76 7. 6.33 1.371 1.236 1.327 1.328 1.438 1.330 1.856 1.989 77 6.613 1.371 1.236 1.327 1.328 1.438 1.330 1.856 1.989 78 6.42 1.678 1.422 1.934 1.238 1.438 1.430 1.856 1.989 80 6.48 1.950 1.1610 2.166 1.881 1.996 1.483 1.310 1.856 1.989 81 6.38 2.125 1.566 2.594 2.135 1.92 1.939 1.956 1.956 1.958 1.999 81 6.38 2.125 1.566 2.594 1.438 1.310 1.856 1.989 81 6.38 2.125 1.566 2.594 1.438 1.950 1.958 1.959 1.958 1.959 1.958 1.958 1.959 1.958 1.	73											
1.50	74	6.20	1.699	1.491	1.907	1.926	143					
77	75	6.05	1.781	1.612		1.537	144	6.67	1.483	1.310		
18	76					1.930	145	6.25	1.666	1.410	1.921	1.621
1989   1982   1983   1422   1994   2192   1488   1.33	77											
80 6 648 1993 1610 2196 1281 149 667 1483 1310 1856 1989 1816 632 1566 1410 1821 1894 182 62 620 1313 1233 1332 1332 1332 1332 1332 13							1					
81 6.38 2.125 1.866 2.594 2.135 150 6.32 1.866 1.410 1.921 1.984 2.620 1.313 1.233 1.332 1.342 1.51 1.624 1.477 1.237 1.567 1.984 2.34 1.51 1.627 1.939 2.34 1.343 1.343 1.473 1.473 1.473 1.520 1.52 6.22 1.504 1.230 1.723 1.508 2.34 1.343 1.473 1.473 1.473 1.520 1.52 6.22 1.504 1.230 1.723 1.508 2.34 1.343												
82         5.20         1.313         1.233         1.322         1.342         151         6.64         1.477         1.267         1.867         1.989           84         6.04         1.273         1.188         1.378         1.290         153         6.52         2.149         1.924         2.374         2.196           85         6.30         1.705         1.383         1.323         1.322         1.416         6.76         2.101         1.32         2.370         1.989           86         6.23         1.313         1.232         1.322         1.447         1.55         6.41         2.602         2.025         3.182         1.788           87         6.27         1.333         1.323         1.344         1.358         1.78         7.18         2.272         2.283         3.182         2.673           88         6.07         1.333         1.223         1.322         1.538         1.79         7.24         2.246         2.291         2.231         2.271         2.280         2.331         2.231         2.231         2.231         2.231         2.232         2.261         3.315         3.292         2.481         2.240         2.224         2.231												
83 6.66 1.315 1.203 1.428 1.473 1.52 6.22 1.594 1.200 1.729 1.590 6.5 6.30 1.705 1.595 1.346 1.529 1.530 1.54 6.56 2.149 1.326 2.374 2.196 6.5 6.30 1.705 1.595 1.346 1.590 1.54 6.76 2.141 1.832 2.370 1.969 6.6 6.2 1.313 1.323 1.322 1.333 1.322 1.333 1.592 1.407 1.55 6.41 2.2463 2.025 3.182 2.573 1.969 6.8 6.23 1.313 1.238 1.328 1.238 1.329 1.238 1.259 1.258 1.259												
84 6.04 1273 1.188 1.378 1.290 153 6.92 2.149 1.924 2.374 2.196 85 6.30 1.705 1.595 1.346 1.595 1.360 154 6.76 2.101 1.82 2.370 1.989 86 6.23 1.313 1.233 1.392 1.308 1.505 6.41 2.603 2.025 3.182 1.788 88 6.07 1.336 1.238 1.233 1.392 1.308 1.505 7.18 2.722 2.233 3.182 2.673 3.88 6.07 1.336 1.258 1.414 1.276 158 7.18 2.722 2.233 3.182 2.673 3.89 6.07 1.336 1.258 1.414 1.276 158 7.48 7.42 2.149 1.924 2.374 2.378 99 6.39 1.313 1.233 1.392 1.536 1.596 1.590 1.590 1.283 2.573 3.89 1.205 1.336 1.258 1.414 1.276 158 7.42 2.409 1.205 1.205 1.505 1.300 1.505 1.300 1.505 1.300 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.405 1.305 1.205 1.205 1.305 1.305 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.205 1.305 1.305 1.205 1.305 1.205 1.305 1.205 1.305 1.205 1.305 1.205 1.305 1.205 1.305 1.305 1.205 1.305 1.205 1.305 1.305 1.205 1.305 1.205 1.305 1.205 1.305 1.305 1.205 1.305 1.205 1.305 1.305 1.205 1.305 1.205 1.305 1.305 1.205 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.205 1.305 1.305 1.305 1.205 1.3												
85 6, 3.0 1,705 1,565 1,846 1,560 1,54 6,76 2,101 1,822 2,370 1,959 6,61 3,131 1,313 1,323 1,392 1,313 1,392 1,313 1,392 1,313 1,392 1,313 1,392 1,313 1,392 1,394 1,395	84											
88 6.23 1.313 1.233 1.392 1.407 1.55 6.41 2.603 2.025 3.182 1.788 87 6.23 1.313 1.233 1.392 1.588 1.67 1.336 1.238 1.238 1.239 1.231 1.392 1.536 1.59 1.71 1.395 1.234 2.2673 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.20 1.30 1.30 1.20 1.30 1.30 1.20 1.30 1.30 1.20 1.30 1.30 1.30 1.20 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.3	85											
88	86	6.23	1.313	1.233	1.392	1.407	155					
89	87	6.29	1.313	1.233	1.392	1.538	156	7.18	2.722	2.263		
99	88					1.276		7.18	2.722	2.263	3.182	
91 6.13 1.336 1.258 1.414 1.248 150 6.33 1.865 1.390 1.950 2.214 1.733 1.168 1.378 1.290 161 7.08 1.865 1.390 1.950 2.457 1.733 1.168 1.378 1.290 162 7.24 2.460 2.091 2.830 2.573 1.950 6.447 1.273 1.168 1.378 1.290 162 7.24 2.460 2.091 2.830 2.573 1.950 6.13 1.273 1.168 1.378 1.248 163 6.99 1.865 1.390 1.950 2.237 1.950 6.13 1.273 1.168 1.378 1.248 164 7.02 1.865 1.390 1.950 2.237 1.950 6.13 1.273 1.168 1.378 1.248 164 7.02 1.865 1.390 1.950 2.238 1.950 6.13 1.233 1.332 1.533 1.532 1.533 1.65 6.93 2.149 1.924 2.374 2.214 1.950 6.23 1.313 1.233 1.332 1.533 1.66 6.93 2.149 1.924 2.374 2.214 1.999 6.13 1.336 1.258 1.144 1.248 167 7.27 2.722 2.223 3.182 2.573 1.999 6.39 1.705 1.555 1.846 1.852 189 1.997 4.231 1.991 1.924 2.374 2.642 1.991	89											
92         6.35         1.315         1.203         1.428         1.540         161         7.08         1.685         1.300         1.990         2.487           93         6.04         1.273         1.188         1.378         1.280         162         7.24         2.60         2.991         2.830         2.573           94         6.13         1.273         1.188         1.378         1.248         183         6.99         1.656         1.300         1.950         2.238           95         6.13         1.273         1.188         1.378         1.248         185         6.99         1.692         1.313         1.950         2.238           96         6.39         1.303         1.258         1.414         1.248         167         7.27         2.272         2.234         2.247           98         6.39         1.705         1.565         1.846         1.892         1.89         1.974         1.940         1.952         2.673           99         6.93         1.705         1.565         1.846         1.892         1.896         1.974         1.914         4.946         2.234         2.467           100         6.23         1.931<												
94 6.13 1.273 1.188 1.378 1.290 152 7.24 2.460 2.091 2.830 2.673 94 6.13 1273 1.168 1.378 1.248 164 7.02 1.665 1.380 1.950 2.378 95 6.13 1.273 1.168 1.378 1.248 164 7.02 1.665 1.380 1.950 2.378 95 6.13 1.273 1.168 1.392 1.538 166 6.59 1.665 1.380 1.950 2.378 97 6.29 1.313 1.233 1.392 1.538 166 6.53 2.149 1.244 2.374 2.214 98 6.13 1.336 1.258 1.414 1.248 167 7.27 2.727 2.226 2.283 3.184 2.2673 99 6.39 1.705 1.565 1.346 1.892 168 7.11 2.149 1.244 2.374 2.642 100 6.23 1.977 1.760 2.195 1.969 169 7.42 3.197 1.399 4.296 3.296 101 6.38 1.313 1.233 1.392 1.532 1.527 170 7.27 2.995 1.347 4.042 2.834 102 6.16 1.336 1.258 1.414 1.849 171 7.11 2.752 2.130 3.373 1.969 103 6.22 1.336 1.258 1.414 1.849 171 7.11 2.752 2.130 3.373 1.969 105 6.65 1.828 1.656 2.160 1.903 174 7.11 2.753 2.741 1.969 106 6.49 1.527 1.337 1.717 2.019 1.75 6.75 1.377 1.777 2.019 1.75 6.76 1.1527 1.375 2.741 1.969 107 6.71 1.527 1.337 1.717 2.019 1.75 6.76 2.170 1.75 2.247 1.75 2.741 1.969 107 6.71 1.527 1.337 1.717 2.019 1.76 6.76 2.173 1.702 2.644 2.122 1.00 6.48 1.313 1.233 1.382 1.253 1.382 1.277 178 2.447 1.186 2.909 1.969												
94 6.13 1.273 1.168 1.378 1.248 163 6.99 1.665 1.380 1.950 2.232 1.955 6.13 1.273 1.168 1.378 1.248 164 7.02 1.665 1.380 1.950 2.237 1.956 5.71 1.406 1.190 1.622 1.643 165 7.05 1.665 1.380 1.950 2.238 1.956 5.71 1.406 1.190 1.622 1.643 165 7.05 1.649 1.465 2.234 2.433 1.950 1.331 1.233 1.233 1.232 1.538 166 6.53 2.149 1.465 2.234 2.234 1.238 1.338 1.238 1.258 1.414 1.248 167 7.27 2.272 2.263 3.182 2.673 1.950 1.05 1.05 1.05 1.05 1.05 1.05 1.965 1.996 169 7.42 3.197 1.399 4.996 2.260 1.06 6.23 1.313 1.233 1.332 1.525 1.527 1.07 7.27 2.95 1.999 4.996 3.296 1.06 6.23 1.336 1.258 1.414 1.446 1.71 7.71 2.77 2.72 2.263 3.387 2.834 1.02 6.16 1.338 1.258 1.414 1.897 1.72 7.27 2.272 2.283 3.387 2.933 1.959 1.00 6.23 1.338 1.258 1.414 1.897 1.72 7.27 2.95 2.130 3.373 1.959 1.00 6.25 1.338 1.258 1.414 1.897 1.72 7.33 2.811 2.130 3.373 1.959 1.05 6.5 1.928 1.699 1.69 7.42 3.197 1.710 2.272 2.274 1.753 2.741 1.959 1.05 6.05 1.928 1.699 1.69 1.72 7.33 2.811 2.136 3.373 1.959 1.05 6.05 1.928 1.699 1.993 1.717 2.019 1.75 7.717 2.247 1.753 2.741 1.959 1.05 6.05 1.928 1.699 1.09 1.00 6.00 1.00 1.00 1.00 1.00 1.00 1.00												
95         6.13         1.273         1.188         1.378         1.248         164         7.02         1.685         1.380         1.990         2.378           96         5.71         1.406         1.190         1.622         1.643         165         7.05         1.849         1.492         2.234         2.433           97         6.29         1.313         1.233         1.352         1.588         166         6.93         2.149         1.924         2.374         2.214           98         6.39         1.705         1.565         1.846         1.892         188         7.11         2.149         1.924         2.374         2.612           100         6.23         1.977         1.760         1.565         1.846         1.892         188         7.11         2.149         1.924         2.374         2.642           101         6.33         1.313         1.233         1.332         1.5277         170         7.27         2.995         1.947         4.042         2.84           102         6.16         1.336         1.258         1.414         1.897         172         7.23         2.811         2.130         3.373         1.991												
98 5.71    1.406												
97 629 1.313 1.223 1.392 1.538 166 6.33 2.149 1.924 2.374 2.214 98 6.13 1.336 1.258 1.414 1.248 167 7.27 2.72 2.263 3.182 2.573 99 6.39 1.705 1.565 1.846 1.892 188 7.11 2.149 1.924 2.374 2.642 100 6.23 1.977 1.760 2.195 1.989 169 169 7.42 3.197 1.389 4.996 3.296 101 6.38 1.313 1.223 1.392 1.527 170 7.27 2.995 1.947 4.042 2.834 102 6.16 1.336 1.258 1.414 1.864 171 7.17 7.27 2.995 1.947 4.042 2.834 103 6.22 1.336 1.258 1.414 1.8897 172 7.33 2.811 2.2136 3.487 2.943 104 5.81 1.679 1.431 1.927 1.649 173 7.02 2.247 1.753 2.741 1.989 105 6.65 1.928 1.696 2.160 1.933 174 7.11 2.247 1.753 2.741 1.989 106 6.64 1.527 1.337 1.717 2.019 175 6.76 2.173 1.702 2.644 2.122 108 6.71 1.527 1.337 1.717 2.019 176 6.76 2.173 1.702 2.644 2.122 108 6.84 1.313 1.223 1.392 1.257 1.78 2.74 1.989 2.999 1.989 109 6.848 1.313 1.223 1.392 1.257 1.78 2.14 1.989 109 6.848 1.313 1.223 1.392 1.257 1.79 1.79 1.79 1.79 1.79 1.79 1.79 1.7												
98 6.13 1.336 1.258 1.414 1.248 167 7.27 2.772 2.723 3.182 2.673 99 6.39 1.705 1.565 1.846 1.892 168 7.11 2.144 1.1924 2.374 2.642 2.010 6.23 1.977 1.760 2.195 1.989 169 7.42 3.197 1.399 4.996 3.296 101 6.33 1.313 1.223 1.382 1.527 170 7.27 2.995 1.947 4.042 2.834 102 6.16 1.336 1.258 1.414 1.464 1.71 7.11 2.752 2.130 3.373 1.989 103 6.22 1.336 1.258 1.414 1.897 172 7.23 2.811 2.238 3.467 2.943 104 5.81 1.679 1.431 1.527 1.809 173 7.02 2.247 1.753 2.741 1.969 105 6.65 1.228 1.696 2.160 1.930 174 7.77 2.019 175 6.76 2.173 7.77 2.247 1.753 2.741 1.969 107 6.71 1.527 1.337 1.717 2.019 175 6.76 2.173 1.702 2.644 2.122 108 6.41 1.337 1.717 2.019 175 6.76 2.173 1.702 2.644 2.122 109 6.48 1.313 1.233 1.332 1.257 178 7.14 2.447 1.986 2.009 1.969 110 6.48 1.313 1.233 1.332 1.257 179 6.73 2.141 1.863 2.419 2.122 111 6.76 1.895 1.386 2.004 2.104 180 7.36 2.995 1.947 4.042 2.998 1113 6.54 1.315 1.203 1.428 1.488 181 7.11 2.752 2.130 3.373 1.969 112 6.45 1.315 1.203 1.428 1.488 181 7.11 2.752 2.130 3.373 1.969 113 6.54 1.315 1.203 1.428 1.488 181 7.11 2.752 2.130 3.373 1.969 115 6.66 2.173 1.702 2.644 2.122 1.257 178 1.44 2.447 1.985 2.490 1.369 1	97											
99 6.39 1.705 1.565 1.846 1.892 168 7.11 2.149 1.924 2.374 2.642 100 6.23 1.977 1.760 2.195 1.999 169 7.42 3.197 1.399 4.996 3.296 101 6.38 1.313 1.233 1.392 1.527 170 7.71 2.295 1.947 4.042 2.834 102 6.16 1.336 1.258 1.414 1.844 171 7.11 2.752 2.130 3.373 1.999 103 6.22 1.336 1.258 1.414 1.897 172 7.33 2.211 2.136 3.487 2.943 105 6.65 1.528 1.896 2.160 1.903 174 7.71 2.247 1.753 2.741 1.993 105 6.65 1.528 1.896 2.160 1.903 174 7.71 2.247 1.753 2.741 1.993 106 6.54 1.527 1.337 1.717 2.019 176 6.76 6.76 1.527 1.337 1.717 2.019 176 6.76 6.76 1.527 1.337 1.717 2.019 177 7.08 2.247 1.753 2.741 1.999 110 6.48 1.313 1.233 1.392 1.257 178 7.74 2.447 1.986 2.999 1.999 110 6.48 1.313 1.233 1.392 1.257 178 6.74 1.943 110 6.76 1.895 1.386 2.004 2.104 180 7.36 2.995 1.947 4.042 2.998 111 6.76 6.76 1.895 1.386 2.004 2.104 180 7.36 2.995 1.947 4.042 2.998 112 6.45 1.315 1.203 1.428 1.488 181 7.11 2.752 2.130 3.373 1.999 115 6.45 1.315 1.203 1.428 1.488 181 7.11 2.752 2.130 3.373 1.999 115 6.45 1.315 1.203 1.428 1.486 181 7.11 2.752 2.130 3.373 1.999 115 6.49 1.755 1.335 1.332 1.332 1.332 1.257 178 6.73 2.141 1.893 2.419 2.122 1.104 6.65 1.315 1.203 1.428 1.488 181 7.11 2.752 2.130 3.373 1.999 115 6.49 1.755 1.755 1.755 1.755 1.755 2.130 3.373 1.999 115 6.49 1.755 1.755 1.335 1.332 1.332 1.332 1.332 1.332 1.332 1.332 1.332 1.333 1.	98											
101	99	6.39	1.705	1.565								
102	100		1.977	1.760	2.195	1.969	169	7.42	3.197	1.399	4.996	3.296
103 6.22 1.336 1.258 1.414 1.897 172 7.33 2.811 2.136 3.487 2.943 104 5.81 1.679 1.431 1.927 1.649 173 7.02 2.247 1.753 2.741 1.969 105 6.85 1.928 1.686 2.160 1.903 174 7.11 2.247 1.753 2.741 1.969 105 6.85 1.928 1.686 2.160 1.903 174 7.11 2.247 1.753 2.741 1.969 106 6.84 1.527 1.337 1.717 2.019 176 6.76 1.717 2.247 1.753 2.741 1.969 109 6.48 1.313 1.233 1.392 1.257 178 7.14 2.447 1.986 2.247 1.753 2.741 1.969 110 6.48 1.313 1.233 1.392 1.257 178 7.14 2.447 1.986 2.999 1.969 110 6.48 1.313 1.233 1.392 1.257 178 7.14 2.447 1.986 2.999 1.969 111 6.67 1.969 1.386 2.004 2.104 180 7.36 2.995 1.947 4.042 2.998 112 6.65 1.315 1.203 1.428 1.488 1.488 181 7.11 2.752 2.30 3.373 1.969 113 6.54 1.315 1.203 1.428 1.428 1.458 1.458 1.451 1.275 2.150 3.373 1.969 113 6.54 1.315 1.203 1.428 1.428 1.472 182 2.720 2.752 2.130 3.373 1.969 115 6.65 1.928 1.896 2.160 1.903 183 7.20 2.752 2.130 3.373 1.969 115 6.49 1.705 1.392 1.595 1.392 1.594 1.592 1.594 1.595 1.396 2.160 1.903 183 7.20 2.752 2.130 3.373 1.969 115 6.49 1.705 1.315 1.203 1.428 1.428 1.472 182 2.247 1.753 2.644 2.000 116 6.53 1.315 1.233 1.392 1.548 1.557 1.548 1.57 1.72 2.474 1.753 2.741 1.999 117 6.66 6.69 2.173 1.702 2.644 2.000 117 6.66 6.69 2.173 1.702 2.644 2.000 118 6.74 1.328 1.666 2.160 2.076 1.77 1.77 2.447 1.753 2.741 1.999 117 6.66 6.69 2.173 1.702 2.644 2.000 118 6.74 1.328 1.666 2.160 2.076 1.77 1.77 2.247 1.753 2.247 1.753 2.741 1.999 117 6.66 6.69 2.173 1.702 2.644 2.2998 118 6.69 2.160 2.076 1.77 1.77 2.247 1.753 2.741 1.999 118 6.54 1.313 1.233 1.392 1.384 1.894 1.896 1.66 6.89 2.173 1.770 2.2444 1.899 1.705 1.565 1.846 1.616 1.88 6.82 2.173 1.770 2.2444 1.369 1.574 1.999 1.565 1.846 1.616 1.88 6.82 2.173 1.770 2.2444 1.299 1.2998 1.206 6.69 2.173 1.770 2.2444 1.2998 1.2998 1.290 1.29	101											
104   5.81   1.679   1.431   1.927   1.849   173   7.02   2.247   1.753   2.741   1.989     105   6.65   1.928   1.896   2.160   1.903   174   7.11   2.247   1.753   2.741   1.989     106   6.64   1.527   1.337   1.717   1.904   175   7.17   2.247   1.753   2.741   1.989     107   6.71   1.527   1.337   1.717   2.019   176   6.76   2.173   1.702   2.644   2.122     108   6.71   1.527   1.337   1.717   2.019   176   6.76   2.143   1.702   2.644   2.122     109   6.48   1.313   1.233   1.392   1.257   179   6.73   2.141   1.863     100   6.48   1.313   1.233   1.392   1.257   179   6.73   2.141   1.863     101   6.48   1.313   1.233   1.392   1.257   179   6.73   2.141   1.863     112   6.45   1.365   1.386   2.004   2.104   180   7.36   2.995   1.947   4.042   2.998     113   6.54   1.315   1.203   1.428   1.468   181   7.11   2.752   2.130   3.373   1.969     114   6.65   1.928   1.696   2.160   1.903   183   7.20   2.752   2.130   3.373   1.969     115   6.49   1.705   1.565   1.846   1.292   1.94   6.85   2.862   2.027   3.697   2.122     116   6.33   1.313   1.233   1.392   1.548   1.964   1.92   2.147   1.753   2.741   1.969     118   6.74   1.928   1.696   2.160   2.076   1.877   7.17   2.247   1.753   2.741   1.969     118   6.74   1.928   1.696   2.160   2.076   187   7.17   2.247   1.753   2.741   1.969     120   6.79   1.527   1.337   1.717   2.144   189   7.71   2.247   1.753   2.741   1.969     121   6.64   1.313   1.233   1.392   1.381   1.90   7.46   2.995   1.947   4.042   2.998     122   6.64   1.313   1.233   1.392   1.381   1.90   7.46   2.995   1.947   4.042   2.998     123   6.74   1.928   1.696   2.160   2.076   1.92   7.52   2.811   2.136   3.487   2.998     123   6.74   1.928   1.696   2.160   2.076   1.97   7.77   2.247   1.753   2.741   1.969     125   6.64   1.313   1.233   1.392   1.381   1.90   7.46   2.995   1.947   4.042   2.998     124   6.65   1.380   1.950   2.168   1.999   2.00   7.52   2.811   2.136   3.487   2.998     125   6.65   1.483   1.391   1.665   1.999   2.00   7.52												
105												
106												
107												
108												
109	108											
110       6.48       1.313       1.233       1.392       1.257       179       6.73       2.141       1.863       2.419       2.122         111       6.76       1.695       1.386       2.004       2.104       178       7.36       2.995       1.947       4.042       2.988         112       6.45       1.315       1.203       1.428       1.468       181       7.11       2.752       2.130       3.373       1.969         113       6.54       1.315       1.203       1.428       1.472       182       7.20       2.752       2.130       3.373       1.969         115       6.49       1.705       1.565       1.846       1.292       184       6.85       2.862       2.027       3.697       2.122         116       6.33       1.313       1.233       1.392       1.548       185       7.11       2.247       1.753       2.741       1.969         117       6.46       1.313       1.233       1.392       1.548       185       7.11       2.247       1.753       2.741       1.969         118       6.74       1.928       1.666       2.160       2.076       187       7.17 <t< td=""><td>109</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	109											
112       6.45       1.315       1.203       1.428       1.468       181       7.11       2.752       2.130       3.373       1.969         113       6.54       1.315       1.203       1.428       1.472       182       7.20       2.752       2.130       3.373       1.969         114       6.65       1.928       1.696       2.160       1.903       183       7.20       2.752       2.130       3.373       1.969         115       6.49       1.705       1.565       1.846       1.292       184       6.85       2.862       2.027       3.697       2.122         116       6.33       1.313       1.233       1.392       1.548       185       7.11       2.247       1.753       2.741       1.969         117       6.46       1.313       1.233       1.392       1.548       185       7.11       2.247       1.753       2.741       1.969         118       6.74       1.928       1.696       2.160       2.076       187       7.17       2.247       1.753       2.741       1.969         119       6.58       1.705       1.565       1.846       1.616       188       6.82 <t< td=""><td>110</td><td>6.48</td><td>1.313</td><td>1.233</td><td>1.392</td><td>1.257</td><td>179</td><td>6.73</td><td>2.141</td><td></td><td></td><td></td></t<>	110	6.48	1.313	1.233	1.392	1.257	179	6.73	2.141			
113       6.54       1.315       1.203       1.428       1.472       182       7.20       2.752       2.130       3.373       1.969         115       6.65       1.928       1.696       2.160       1.903       183       7.20       2.752       2.130       3.373       1.969         115       6.49       1.705       1.565       1.846       1.292       184       6.85       2.862       2.027       3.697       2.122         116       6.33       1.313       1.233       1.392       1.548       185       7.11       2.247       1.753       2.741       1.969         117       6.46       1.313       1.233       1.392       1.388       186       6.69       2.173       1.702       2.264       2.080         118       6.74       1.928       1.696       2.160       2.076       187       7.17       2.247       1.753       2.741       1.969         119       6.58       1.705       1.565       1.846       1.616       188       6.82       2.173       1.702       2.644       2.122         120       6.79       1.527       1.337       1.717       2.144       189       7.71 <t< td=""><td>111</td><td></td><td></td><td></td><td></td><td></td><td>180</td><td>7.36</td><td>2.995</td><td></td><td></td><td>2.998</td></t<>	111						180	7.36	2.995			2.998
114       6.65       1.928       1.696       2.160       1.903       183       7.20       2.752       2.130       3.373       1.969         115       6.49       1.705       1.565       1.246       1.292       184       6.85       2.862       2.027       3.697       2.122         116       6.33       1.313       1.233       1.392       1.548       185       7.11       2.247       1.753       2.741       1.969         117       6.46       1.313       1.233       1.392       1.398       186       6.69       2.173       1.702       2.644       2.080         118       6.74       1.928       1.896       2.160       2.076       187       7.17       2.247       1.753       2.741       1.969         119       6.58       1.705       1.565       1.846       1.616       188       6.82       2.173       1.702       2.644       2.122         120       6.79       1.527       1.337       1.717       2.144       189       7.71       3.224       1.278       5.171       2.673         121       6.64       1.527       1.337       1.717       1.904       191       7.55 <t< td=""><td>112</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>	112											
115       6.48       1.705       1.565       1.846       1.292       184       6.85       2.862       2.027       3.697       2.122         116       6.33       1.313       1.233       1.392       1.548       185       7.11       2.247       1.753       2.741       1.969         117       6.46       1.313       1.233       1.392       1.398       186       6.69       2.173       1.702       2.644       2.080         118       6.74       1.928       1.696       2.160       2.076       187       7.17       2.247       1.753       2.741       1.969         119       6.58       1.705       1.565       1.846       1.616       188       6.82       2.173       1.702       2.644       2.122         120       6.79       1.527       1.337       1.717       2.144       189       7.71       3.224       1.278       5.171       2.673         121       6.64       1.527       1.337       1.717       1.904       191       7.55       2.995       1.947       4.042       2.998         122       6.64       1.527       1.337       1.717       2.057       193       7.52 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>												
116       6.33       1.313       1.233       1.392       1.548       185       7.11       2.247       1.753       2.741       1.969         117       6.46       1.313       1.233       1.392       1.398       186       6.69       2.173       1.702       2.644       2.080         118       6.74       1.928       1.696       2.160       2.076       187       7.17       2.247       1.753       2.741       1.969         119       6.58       1.705       1.565       1.846       1.616       188       6.82       2.173       1.702       2.644       2.122         120       6.79       1.527       1.337       1.717       2.144       189       7.71       3.224       1.278       5.171       2.673         121       6.64       1.313       1.233       1.392       1.831       190       7.46       2.995       1.947       4.042       2.998         122       6.64       1.527       1.337       1.717       1.904       191       7.55       2.995       1.947       4.042       2.998         123       6.74       1.928       1.696       2.160       2.076       192       7.52 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>												
117       6.46       1.313       1.233       1.392       1.398       186       6.69       2.173       1.702       2.644       2.000         118       6.74       1.928       1.696       2.160       2.076       187       7.17       2.247       1.753       2.741       1.969         119       6.58       1.705       1.565       1.846       1.616       188       6.82       2.173       1.702       2.644       2.122         120       6.79       1.527       1.337       1.717       2.144       189       7.71       3.224       1.278       5.171       2.673         121       6.64       1.313       1.233       1.392       1.831       190       7.46       2.995       1.947       4.042       2.998         122       6.64       1.527       1.337       1.717       1.904       191       7.55       2.995       1.947       4.042       2.998         122       6.64       1.527       1.337       1.717       1.904       191       7.55       2.995       1.947       4.042       2.998         123       6.74       1.928       1.666       2.160       2.076       192       7.52 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>												
118       6.74       1.928       1.696       2.160       2.076       187       7.17       2.247       1.753       2.741       1.969         119       6.58       1.705       1.565       1.846       1.616       188       6.82       2.173       1.702       2.644       2.122         120       6.79       1.527       1.337       1.717       2.144       189       7.71       3.224       1.278       5.171       2.673         121       6.64       1.313       1.233       1.392       1.831       190       7.46       2.995       1.947       4.042       2.998         122       6.64       1.527       1.337       1.717       1.904       191       7.55       2.995       1.947       4.042       2.998         123       6.74       1.928       1.696       2.160       2.076       192       7.52       2.811       2.136       3.487       2.998         124       6.73       1.527       1.337       1.717       2.057       193       7.52       2.811       2.136       3.487       2.998         125       6.51       1.313       1.233       1.392       1.364       194       7.80 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>												
119       6.58       1.705       1.565       1.846       1.616       188       6.82       2.173       1.702       2.644       2.122         120       6.79       1.527       1.337       1.717       2.144       189       7.71       3.224       1.278       5.171       2.673         121       6.64       1.313       1.233       1.392       1.831       190       7.46       2.995       1.947       4.042       2.998         122       6.64       1.527       1.337       1.717       1.904       191       7.55       2.995       1.947       4.042       2.998         123       6.74       1.928       1.696       2.160       2.076       192       7.52       2.811       2.136       3.487       2.998         124       6.73       1.527       1.337       1.717       2.057       193       7.52       2.811       2.136       3.487       2.998         125       6.51       1.313       1.233       1.392       1.364       194       7.80       3.260       1.089       5.431       2.998         125       6.51       1.313       1.233       1.3208       2.637       195       7.56       <	118											
120       6.79       1.527       1.337       1.717       2.144       189       7.71       3.224       1.278       5.171       2.673         121       6.64       1.313       1.233       1.392       1.831       190       7.46       2.995       1.947       4.042       2.998         122       6.64       1.527       1.337       1.717       1.904       191       7.55       2.995       1.947       4.042       2.998         123       6.74       1.928       1.696       2.160       2.076       192       7.52       2.811       2.136       3.487       2.998         124       6.73       1.527       1.337       1.717       2.057       193       7.52       2.811       2.136       3.487       2.998         125       6.51       1.313       1.233       1.392       1.364       194       7.80       3.260       1.089       5.431       2.998         126       6.89       2.709       2.210       3.208       2.637       195       7.56       3.214       1.318       5.111       1.969         127       6.95       2.464       2.184       2.745       2.444       196       7.65 <t< td=""><td>119</td><td>6.58</td><td>1.705</td><td>1.565</td><td>1.846</td><td></td><td></td><td></td><td></td><td></td><td>2.644</td><td></td></t<>	119	6.58	1.705	1.565	1.846						2.644	
121       6.64       1.313       1.233       1.392       1.831       190       7.46       2.995       1.947       4.042       2.998         122       6.64       1.527       1.337       1.717       1.904       191       7.55       2.995       1.947       4.042       2.998         123       6.74       1.928       1.696       2.160       2.076       192       7.52       2.811       2.136       3.487       2.998         124       6.73       1.527       1.337       1.717       2.057       193       7.52       2.811       2.136       3.487       2.998         125       6.51       1.313       1.233       1.392       1.364       194       7.80       3.260       1.089       5.431       2.998         126       6.89       2.709       2.210       3.208       2.637       195       7.56       3.214       1.318       5.111       1.969         127       6.95       2.464       2.184       2.745       2.444       196       7.65       3.214       1.318       5.111       1.969         129       6.73       1.665       1.380       1.950       2.154       198       7.62 <t< td=""><td>120</td><td>6.79</td><td>1.527</td><td>1.337</td><td>1.717</td><td>2.144</td><td>189</td><td>7.71</td><td>3.224</td><td>1.278</td><td>5.171</td><td>2.673</td></t<>	120	6.79	1.527	1.337	1.717	2.144	189	7.71	3.224	1.278	5.171	2.673
123       6.74       1.928       1.696       2.160       2.076       192       7.52       2.811       2.136       3.487       2.998         124       6.73       1.527       1.337       1.717       2.057       193       7.52       2.811       2.136       3.487       2.998         125       6.51       1.313       1.233       1.392       1.364       194       7.80       3.260       1.089       5.431       2.998         126       6.89       2.709       2.210       3.208       2.637       195       7.56       3.214       1.318       5.111       1.969         127       6.95       2.464       2.184       2.745       2.444       196       7.65       3.214       1.318       5.111       1.969         128       6.74       2.149       1.924       2.374       2.190       197       7.30       3.188       1.417       4.959       2.122         129       6.73       1.665       1.380       1.950       2.154       198       7.62       3.162       1.525       4.800       1.969         130       6.80       1.665       1.380       1.950       2.186       199       7.20 <t< td=""><td>121</td><td></td><td>1.313</td><td>1.233</td><td>1.392</td><td></td><td></td><td>7.46</td><td>2.995</td><td>1.947</td><td>4.042</td><td>2.998</td></t<>	121		1.313	1.233	1.392			7.46	2.995	1.947	4.042	2.998
124       6.73       1.527       1.337       1.717       2.057       193       7.52       2.811       2.136       3.487       2.998         125       6.51       1.313       1.233       1.392       1.364       194       7.80       3.260       1.089       5.431       2.998         126       6.89       2.709       2.210       3.208       2.637       195       7.56       3.214       1.318       5.111       1.969         127       6.95       2.464       2.184       2.745       2.444       196       7.65       3.214       1.318       5.111       1.969         128       6.74       2.149       1.924       2.374       2.190       197       7.30       3.188       1.417       4.959       2.122         129       6.73       1.665       1.380       1.950       2.154       198       7.62       3.162       1.525       4.800       1.969         130       6.80       1.665       1.380       1.950       2.186       199       7.20       3.037       1.856       4.218       2.122         131       6.58       1.483       1.310       1.656       1.969       200       7.27 <t< td=""><td>122</td><td></td><td></td><td></td><td>1.717</td><td></td><td></td><td></td><td></td><td>1.947</td><td>4.042</td><td></td></t<>	122				1.717					1.947	4.042	
125         6.51         1.313         1.233         1.392         1.364         194         7.80         3.260         1.089         5.431         2.998           126         6.89         2.709         2.210         3.208         2.637         195         7.56         3.214         1.318         5.111         1.969           127         6.95         2.464         2.184         2.745         2.444         196         7.65         3.214         1.318         5.111         1.969           128         6.74         2.149         1.924         2.374         2.190         197         7.30         3.188         1.417         4.959         2.122           129         6.73         1.665         1.380         1.950         2.154         198         7.62         3.162         1.525         4.800         1.969           130         6.80         1.665         1.380         1.950         2.186         199         7.20         3.037         1.856         4.218         2.122           131         6.58         1.483         1.310         1.656         1.969         200         7.27         3.037         1.856         4.218         2.122					2.160				2.811			
126       6.89       2.709       2.210       3.208       2.637       195       7.56       3.214       1.318       5.111       1.969         127       6.95       2.464       2.184       2.745       2.444       196       7.65       3.214       1.318       5.111       1.969         128       6.74       2.149       1.924       2.374       2.190       197       7.30       3.188       1.417       4.959       2.122         129       6.73       1.665       1.380       1.950       2.154       198       7.62       3.162       1.525       4.800       1.969         130       6.80       1.665       1.380       1.950       2.186       199       7.20       3.037       1.856       4.218       2.122         131       6.58       1.483       1.310       1.656       1.969       200       7.27       3.037       1.856       4.218       2.122         132       6.58       1.483       1.310       1.656       1.969       201       7.62       3.162       1.525       4.800       1.969         133       6.86       1.849       1.465       2.234       1.962       202       7.24 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>												
127         6.95         2.464         2.184         2.745         2.444         196         7.65         3.214         1.318         5.111         1.969           128         6.74         2.149         1.924         2.374         2.190         197         7.30         3.188         1.417         4.959         2.122           129         6.73         1.665         1.380         1.950         2.154         198         7.62         3.162         1.525         4.800         1.969           130         6.80         1.665         1.380         1.950         2.186         199         7.20         3.037         1.856         4.218         2.122           131         6.58         1.483         1.310         1.656         1.969         200         7.27         3.037         1.856         4.218         2.122           132         6.58         1.483         1.310         1.656         1.969         201         7.62         3.162         1.525         4.800         1.969           133         6.86         1.849         1.465         2.234         1.962         202         7.24         3.100         1.681         4.520         2.122					1.37Z 2.200				3.20U 2.214			
128         6.74         2.149         1.924         2.374         2.190         197         7.30         3.188         1.417         4.959         2.122           129         6.73         1.665         1.380         1.950         2.154         198         7.62         3.162         1.525         4.800         1.969           130         6.80         1.665         1.380         1.950         2.186         199         7.20         3.037         1.856         4.218         2.122           131         6.58         1.483         1.310         1.656         1.969         200         7.27         3.037         1.856         4.218         2.122           132         6.58         1.483         1.310         1.656         1.969         201         7.62         3.162         1.525         4.800         1.969           133         6.86         1.849         1.465         2.234         1.962         202         7.24         3.100         1.681         4.520         2.122           134         6.55         1.477         1.287         1.667         1.969         203         7.65         3.214         1.318         5.111         1.969												
129       6.73       1.665       1.380       1.950       2.154       198       7.62       3.162       1.525       4.800       1.969         130       6.80       1.665       1.380       1.950       2.186       199       7.20       3.037       1.856       4.218       2.122         131       6.58       1.483       1.310       1.656       1.969       200       7.27       3.037       1.856       4.218       2.122         132       6.58       1.483       1.310       1.656       1.969       201       7.62       3.162       1.525       4.800       1.969         133       6.86       1.849       1.465       2.234       1.962       202       7.24       3.100       1.681       4.520       2.122         134       6.55       1.477       1.287       1.667       1.969       203       7.65       3.214       1.318       5.111       1.969         135       6.64       1.477       1.287       1.667       1.969       204       7.30       3.188       1.417       4.959       2.112         136       6.22       1.504       1.280       1.729       1.590       205       8.00 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>												
130       6.80       1.665       1.380       1.950       2.186       199       7.20       3.037       1.856       4.218       2.122         131       6.58       1.483       1.310       1.656       1.969       200       7.27       3.037       1.856       4.218       2.122         132       6.58       1.483       1.310       1.656       1.969       201       7.62       3.162       1.525       4.800       1.969         133       6.86       1.849       1.465       2.234       1.962       202       7.24       3.100       1.681       4.520       2.122         134       6.55       1.477       1.287       1.667       1.969       203       7.65       3.214       1.318       5.111       1.969         135       6.64       1.477       1.287       1.667       1.969       204       7.30       3.188       1.417       4.959       2.112         136       6.22       1.504       1.280       1.729       1.590       205       8.00       3.260       1.089       5.431       2.998         137       6.83       2.149       1.924       2.374       2.184       206       8.09 <t< td=""><td></td><td></td><td></td><td></td><td>1.950</td><td></td><td></td><td></td><td>3,162</td><td>1.525</td><td>4.800</td><td></td></t<>					1.950				3,162	1.525	4.800	
131       6.58       1.483       1.310       1.656       1.969       200       7.27       3.037       1.856       4.218       2.122         132       6.58       1.483       1.310       1.656       1.969       201       7.62       3.162       1.525       4.800       1.969         133       6.86       1.849       1.465       2.234       1.962       202       7.24       3.100       1.681       4.520       2.122         134       6.55       1.477       1.287       1.667       1.969       203       7.65       3.214       1.318       5.111       1.969         135       6.64       1.477       1.287       1.667       1.969       204       7.30       3.188       1.417       4.959       2.122         136       6.22       1.504       1.280       1.729       1.590       205       8.00       3.260       1.089       5.431       2.998         137       6.83       2.149       1.924       2.374       2.184       206       8.09       3.272       1.001       5.544       1.969         138       6.83       2.149       1.924       2.374       2.184       207       7.74 <t< td=""><td></td><td></td><td>1.665</td><td></td><td>1.950</td><td>2.186</td><td></td><td></td><td>3.037</td><td>1.856</td><td></td><td></td></t<>			1.665		1.950	2.186			3.037	1.856		
132     6.58     1.483     1.310     1.656     1.969     201     7.62     3.162     1.525     4.800     1.969       133     6.86     1.849     1.465     2.234     1.962     202     7.24     3.100     1.681     4.520     2.122       134     6.55     1.477     1.287     1.667     1.969     203     7.65     3.214     1.318     5.111     1.969       135     6.64     1.477     1.287     1.667     1.969     204     7.30     3.188     1.417     4.959     2.122       136     6.22     1.504     1.280     1.729     1.590     205     8.00     3.260     1.089     5.431     2.998       137     6.83     2.149     1.924     2.374     2.184     206     8.09     3.272     1.001     5.544     1.969       138     6.83     2.149     1.924     2.374     2.184     207     7.74     3.269     1.027     5.511     2.122       139     6.67     2.101     1.832     2.370     1.969     208     7.71     3.264     1.064     5.464     2.122	131	6.58	1.483		1.656	1.969		7.27	3.037	1.856		2.122
134     6.55     1.477     1.287     1.667     1.969     203     7.65     3.214     1.318     5.111     1.969       135     6.64     1.477     1.287     1.667     1.969     204     7.30     3.188     1.417     4.959     2.122       136     6.22     1.504     1.280     1.729     1.590     205     8.00     3.260     1.089     5.431     2.998       137     6.83     2.149     1.924     2.374     2.184     206     8.09     3.272     1.001     5.544     1.969       138     6.83     2.149     1.924     2.374     2.184     207     7.74     3.269     1.027     5.511     2.122       139     6.67     2.101     1.832     2.370     1.969     208     7.71     3.264     1.064     5.464     2.122					1.656			7.62	3.162	1.525	4.800	
135     6.64     1.477     1.287     1.667     1.969     204     7.30     3.188     1.417     4.959     2.122       136     6.22     1.504     1.280     1.729     1.590     205     8.00     3.260     1.089     5.431     2.998       137     6.83     2.149     1.924     2.374     2.184     206     8.09     3.272     1.001     5.544     1.969       138     6.83     2.149     1.924     2.374     2.184     207     7.74     3.269     1.027     5.511     2.122       139     6.67     2.101     1.832     2.370     1.969     208     7.71     3.264     1.064     5.464     2.122									3.100			
136     6.22     1.504     1.280     1.729     1.590     205     8.00     3.260     1.089     5.431     2.998       137     6.83     2.149     1.924     2.374     2.184     206     8.09     3.272     1.001     5.544     1.969       138     6.83     2.149     1.924     2.374     2.184     207     7.74     3.269     1.027     5.511     2.122       139     6.67     2.101     1.832     2.370     1.969     208     7.71     3.264     1.064     5.464     2.122					1.667				3.214			
137     6.83     2.149     1.924     2.374     2.184     206     8.09     3.272     1.001     5.544     1.969       138     6.83     2.149     1.924     2.374     2.184     207     7.74     3.269     1.027     5.511     2.122       139     6.67     2.101     1.832     2.370     1.969     208     7.71     3.264     1.064     5.464     2.122					1.667				3.188			
138     6.83     2.149     1.924     2.374     2.184     207     7.74     3.269     1.027     5.511     2.122       139     6.67     2.101     1.832     2.370     1.969     208     7.71     3.264     1.064     5.464     2.122									3.26U 2.272			
139 6.67 2.101 1.832 2.370 1.969 208 7.71 3.264 1.064 5.464 2.122					2.314 2.37A							
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Abbreviations: IUPAC, International Union of Pure and Applied Chemistry; E50, the concentration producing an activity 50% above the control activity; CL, 95% confidence limit. The Bayes estimates of log E50 are also shown.

104.3  $\mu$ M, respectively. Based on dose addition, the second order logistic model predicted 25.7, 32.0, and 69.3  $\mu$ M for the E50 of these mixtures, respectively. Based on dose addition, the EBE predicted 35.4, 43.6, and 96.3  $\mu$ M, respectively. The EBEs provide better predictions of mixture E50s; this suggests that the model is attributing to error important details of the structural relationship contained in the estimated log E50s.

### **Discussion**

Adequacy of the concentration-activity model. A logistic model was fit to the activity-concentration data; the estimation of the maximum was unstable so an exponential model was used instead. This model is similar to the logistic, but it has no maximum. In fitting the exponential, we deleted data at high concentrations when the activity decreased with increasing concentration. This reversal in slope might indicate that the concentration-activity curve has reached a maximum and, for some congeners, the activity might never attain 50% above control. However, the congener could metabolize to a more soluble metabolite, justifying this deletion of data. On the other hand, congeners whose activity does not attain 50% above control might be considered inert with respect to the E50, but, for example, active with respect to the E10. Whether the congener is inert or weakly active is difficult to discern; however, this distinction is of less concern in mixture prediction.

Adequacy and validation of the model relating activity to structure. One objective of this study was to determine how reliable the predictions were for the untested congeners. The internal validation was very good with a  $Q^2 = 0.641$ . The use of a logistic model to describe the relationship between activity and chemical structure was very successful. The graph of the logistic model is a sigmoidal-shaped curve, so the range of predictions from this model is between two fixed parameters. Therefore, the prediction of extreme E50 values is avoided. The use of the logistic model causes the smallest E50 prediction to be near the average of other small E50s, rather than possibly being a value lower than any calculated E50. Because our model is empirical, this reluctance to extrapolate is reasonable. Logistic regression in this instance is very similar to discriminant analysis with two classes—active and inactive congeners.

There were indications of lack of fit of the model. In this case, one might predict the mixtures with the estimated E50s rather than the predictions from the logistic model. This strategy only works for tested congeners, and we still need a way to

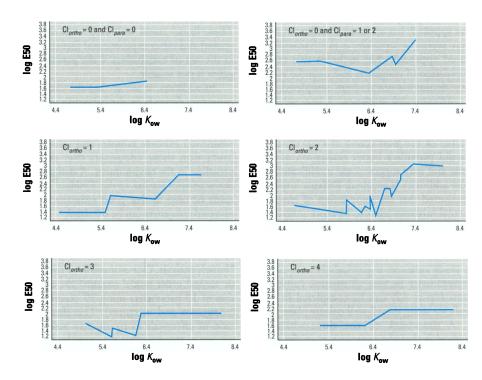


Figure 5. Bayes estimates of log E50 versus log  $K_{ow}$ . E50, the concentration producing an activity 50% above the control activity.

predict the E50s of the untested congeners. The EBE offers a compromise in this case. The EBE shrinks the estimated E50s toward the model-predicted E50s based on the amount of lack of fit. Then the EBEs for the untested congeners were obtained by straight line connections of these points when plotted versus  $\log K_{\rm ow}$ .

There are various ways this process could be improved. We want to evaluate both prediction methods using various types of PCB environmental mixtures before we decide which prediction method is best.

Comparison to other approaches for determining structure-activity relationships. It is enlightening to compare this approach with structure-activity modeling using Hansch analysis as described by Martin (21). Martin believes "the Hansch method is most suitable for a data set that has the following characteristics: 1) the compounds should be structural analogs that are identical in the structure of the pharmacopone, 2) all analogs should produce their biological effect by interacting with the same biological receptor(s), 3) it should be possible to derive quantitative measures of the physical properties of the analogs, 4) there should be enough compounds in the set that one can statistically examine a number of properties, . . . 5) the variation in potency between different analogs should be substantially larger than the error in measuring potency, and 6) the relevant physicochemical properties should be varied properly within the series."

It is not clear that the 209 PCB congeners satisfy the Hansch assumptions. They do not all interact with the same receptor. This generally requires the dose-response slopes to be equal. We have fit the activity curves with the same slope, and this is a good approximation at this stage. More congeners should be tested to determine whether the slopes vary with subsets of the congeners. Thus, there is a lack of evidence to conclude that the slopes differ or that the shapes of the concentration-activity curves are not similar. On the other hand, there is increasing evidence that not all congeners interact with the same receptors. Therefore, PCB congeners may not satisfy this assumption, and Hansch analysis may not be appropriate. However, Hansch analysis may be appropriately applied to subsets of the 209 congeners once those subsets that satisfy the assumptions have been identified.

We have previously stated why we did not use mechanistically based variables in our model. However, Verhaar et al. (22) have shown an advantage of using mechanistically based variables in risk assessments of those complex mixtures in the environment whose chemical components are difficult to measure. Those interested in such approaches may find our predicted E50s useful to relate to mechanistically based variables.

Because this is an empirical approach, there are limitations. One cannot be as comfortable in the predictability from an empirical approach as from an approach that uses mechanistically based variables. However, this approach has achieved a prediction error that seems acceptable; a mechanistically based approach that includes this target population of congeners and a similar activity endpoint has not yet been completed.

Mixture risk assessment. A very practical approach to predict PCB mixture activity is to use the dose-addition assumption. Future studies of the joint action of PCB mixtures should provide a better evaluation of this issue and may suggest some modification to dose additivity is required. Perhaps it will be discovered that the joint action of environmental mixtures tends to be more antagonistic on average. A simple correction could be introduced to account for this deviation from additivity. The use of this test system to study mixtures is particularly sensitive to nonadditivity because all mixture combinations (up to 12) can be completed in one replicate using the 12-well culture plate.

A drawback to the dose-addition method is that the components of the mixture need to be known, and this information can be difficult to obtain for some complex mixtures in the environment. However, if one knows the percent of chlorine in a PCB mixture, this and other knowledge could be used to calculate a probability interval for the E50 of an environmental PCB mixture that would be useful in determining risk. This calculation would be based on predicted E50s as we have provided and might require the assumption of a probability distribution for PCB congeners.

Congener selection. Tysklind et al. (23) discussed a procedure for selecting PCB congeners for use in quantitative structure-activity modeling. They restricted the congeners to the 154 tetra- through hepta-chlorinated congeners. Some restriction is necessary in view of the solubility problems encountered with most of the test systems. The congeners were described using 47 physicochemical variables, and principal component analysis reduced the number of variables to four orthogonal summary variables. The full 24 factorial design plus four center points required 20 congeners to be tested. These 20 congeners were divided into two groups. One group of 10 congeners was labeled the training set to be used for model development. The second group was labeled the validation set. The division occurred so that both sets of congeners typified the whole chemical domain of the four summary variables.

Given our goal of mixture prediction and the problems encountered with solubility, the approach considered by Tysklind et al. (23) does not seem appropriate. It is efficient to restrict testing to those congeners that are soluble, as their approach does. However, some sampling needs to be done to determine the limits of that region. These limits could well vary with the test system and other experimental factors, such as the use of metabolites if the parent congener is not soluble.

In addition, it seems that the choice of congeners depends on the balancing of several objectives. For example, we can test those congeners found in high percentages in environmental mixture samples and reserve for prediction those congeners that are less prevalent in the environment. A design with characteristics similar to the Tysklind design could be used so that good estimates of the untested congeners can be obtained.

Do more congeners need to be tested? Martin (21) has suggested that a 3 to 1 ratio of chemicals to parameters be used for Hansch analysis. Our estimation of the logistic second order model required the estimation of 13 parameters using 39 observations (congeners and mixtures). Therefore, our ratio of chemicals to parameters meets the minimum requirements suggested by Martin (21). In the area of general medical research, which is probably subject to more sources of prediction error than QSAR, Neter et al. (24) have suggested the use of a 6 to 1 ratio as a rule of thumb. Our more modest goal of prediction and description rather than variable selection may not require as large a ratio. Also, our use of the logistic model reduces the range of prediction. This reduction in range should limit the prediction error, which should translate into a less stringent requirement for precise estimates of the regression coefficients. The precision of these estimates is the reason for requiring a high ratio of chemicals to variables.

We think we have tested enough congeners. We have tried to externally validate various models based upon data from 17, 24, and 28 congeners. As the number of congeners fit to the model increased, the relative number of prediction errors decreased. The width of the confidence intervals as shown in Table 4 depend upon the fit of the model and how well the tested congeners span the space of the untested target congeners. Testing more congeners to better span the space of the target congeners is not likely to yield smaller confidence intervals due to insolubility limitations. Testing more congeners to justify the use of a more biologically based model such as a main effect model does not seem productive. Therefore, no further single congener testing using this test system is planned.

Further testing of mixtures is planned, however. We have tested a few other mixtures and expect to learn some new information about mixtures. When the model is fit to E50s arising mainly from mixture testing rather than from single congener

testing, we initially expect a worsening of the fit of the model. This is due to information that the present model does not consider. For example, solubility might not have a dose-addition joint action and would interfere less in data consisting mainly of mixtures. After this phase has passed and enough mixtures have been tested, we expect the model to provide satisfactory predictions of mixtures.

Risk assessment implications. Although further research is needed to better understand whether this test system (PKC activation/translocation) has any role in the neurotoxicity of PCBs, data from this test system eventually may be used in terms of assessing the biological activity of PCB mixtures in a risk assessment. It is believed that this analysis of the data could provide benchmark estimates for mixtures following the method used by Crump (25) with some modifications. These modifications may include the method used to calculate confidence limits, the need for a lower bound on the slope estimate, and the use of a concentration causing a percentage of subjects to be affected rather than the E50.

# Conclusion

This approach toward prediction and relating structure to activity is novel in several ways. The laboratory effort is reduced because our exponential model does not have the data requirement of estimating a maximum. The model has been validated, but there were indications of lack of fit. Also, the predictions of E50s for the three commercial mixtures based on dose addition were lower than the estimated E50s. Future mixture studies should indicate how the dose-additivity equation needs to be modified to predict various environmental mixtures. Our empirical approach is not limited to the assumptions of Hansch analysis. This approach, suitably modified, should be useful when applied to other test systems and should improve the ability to evaluate PCB congeners for hazard identification.

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